

## The ideal pop-pop engine

The ideal (theoretical) pop-pop engine is provided with an evaporator of minimum volume, and the stroke of the liquid piston is maximum; i.e. at the top dead center the gas volume is null and at the bottom dead center it fills the whole pipe. In other words, with following notations:

S=cross section area of the pipe.

L=pipe length.

$\rho$ =specific gravity of water.

- The mean gas volume is half the one of the pipe.  $V=1/2 SL$
- The mean mass of the moving water is  $M=1/2 \rho SL$

Knowing that the pressure inside the evaporator is close to atmospheric pressure, and that the mean temperature of the moving water is slightly above the tank one, we will use for the calculations  $P=10^5\text{Pa}$  and  $\rho=1000\text{kg/m}^3$ .

With legal units (L in m and S in  $\text{m}^2$ ) and considering that the natural frequency of the engine is the one of a classic resonator, we get:

The frequency (Hz)  $F = \frac{1}{2\pi} \sqrt{\frac{P \cdot S^2}{MV}} = \frac{10}{\pi L}$  which depends only on the pipe length.

The maximum thrust (N)  $T = \frac{\rho \pi^2}{4S} (SLF)^2 = \frac{10^5}{4} S$  which depends only on the cross section.

Reminder: this concerns only the “ideal” engine; i.e. without steam drum.

Let’s compare theory with the results of some of our best engines.

Pipe inner diameter (mm)	Theoretical max frequency (Hz)	Measured frequency (Hz)
4 (L=300)	10,6	8
6 (L=480)	6,6	5
8,2 (L=580)	5,5	3
12 (L=745)	4,3	2,4

Roughly, the measured frequencies correspond to the calculated ones. However, they all are lower than the maximum theoretical value. The reason (among others?) is the fact the evaporator volume is not negligible. At the top dead center it remains some gas. We could observe this on many occasions with transparent engines.

For the thrust the results are more disappointing.

Pipe inner diameter (mm)	Theoretical max thrust (mN)	Measured thrust (mN)
4	314	17
6	707	44
8,2	1320	48
12	2827	72

In addition, we know that the thrust measuring device we used indicates slightly more than the actual value (see “Why do we measure more than the theory?”).

Causes of error:

- Actual stroke shorter than L.

According to our visual observations this could explain a ratio of approx 2 for small engines. We don't know how much for big ones.

- Actual frequency lower than the theoretical value.

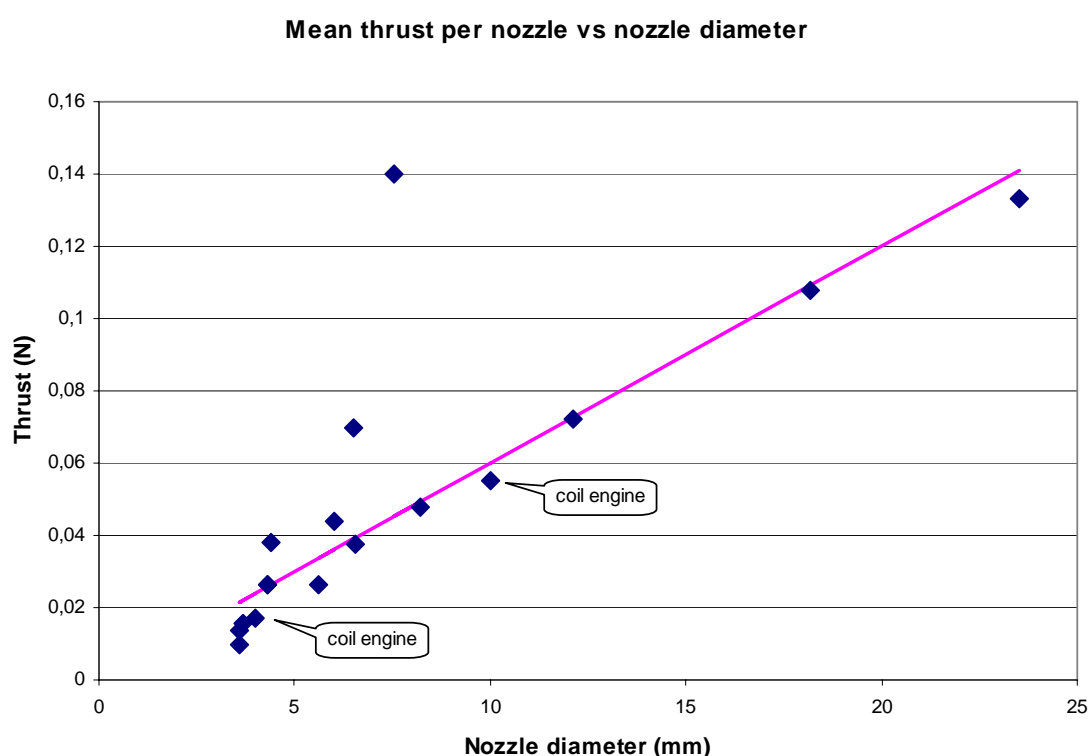
Intervenes as the square. Could justify a ratio of approx 3. Combined with the previous one, ( $2 \times 3 = 6$ ) we still are far from the reality for a small engine.

- Too optimistic assumptions.
- Others???? (Emulsion, specific gravity lower than  $1000\text{kg/m}^3$ ...)

Therefore, the ideal pop-pop engine doesn't exist.

For what concerns the frequency, we could get a lower result by using a big evaporator, but in the other way it is impossible to get a frequency higher than the theoretical value as defined by the previous formula.

For what concerns the thrust, it increases with the pipe diameter. It can be seen on the following graph.



Note: what is called "mean thrust" is the average of a 15 minute record. Instantaneous thrusts up to 30 times higher than the average were recorded, but they are rare and they don't influence the average because they are generally followed by several seconds with no visible thrust.

This graph sets as evident a quasi-linearity between the diameter (in abscissa) and the thrust (in ordinate), but not between section and thrust as I expected. That's a pity!

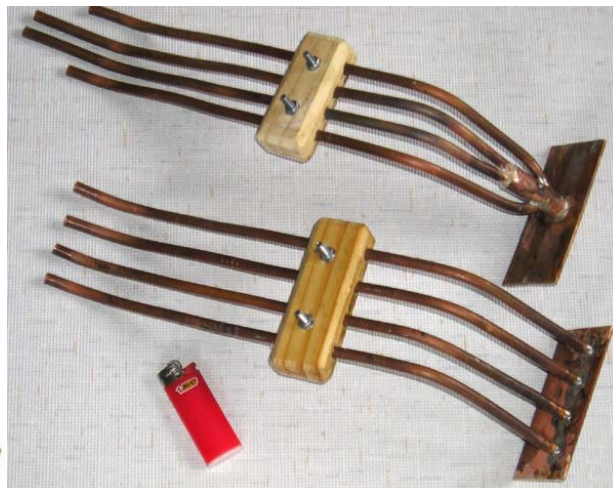
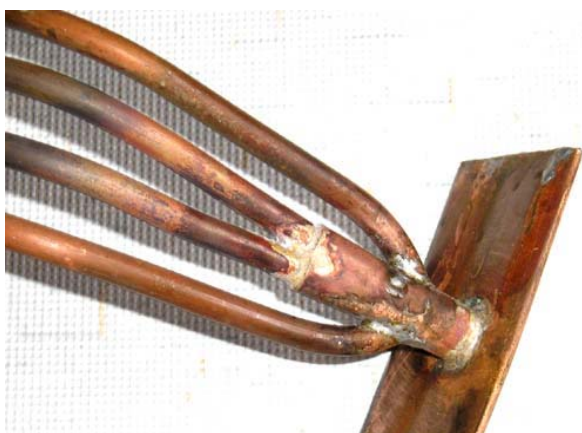
Consequently, two pipes of section S are more performing than a single pipe of section 2S. Even though this disappoints me, it seems evident at this knowledge level. The Burmese boat with 3 pipes, or Daryl's one with 4 pipes are interesting tracks we have to follow. Since that time, I have built engines with up to 8 pipes and Daryl built up to 10.

My feeling is that the theory of the resonator is not so bad. The main problem is at the thermodynamics level. How could we excite a big resonator to get a long stroke? The difficulty comes from the fact everything doesn't follow the scaling factor. For instance, on one side the mass increases as the cube while the area increases only as the square. On the other side, cooling is ensured mainly by the pipe and by the thin layer of water during the climbing down of the water snake. We have to work on the evaporator.



On a single pipe engine I tried an evaporator with pipes inside to increase the area of the hot source. Nothing bad or good to report.

Then I tried to compare two 4 pipe engines, one with a manifold and one with individual connections to the evaporator. No visible difference in thrust.



Since that time, we are working on different basic designs.

To be continued...

## Optimum shape of a pop-pop engine?

(For rigid engines not for diaphragm ones)

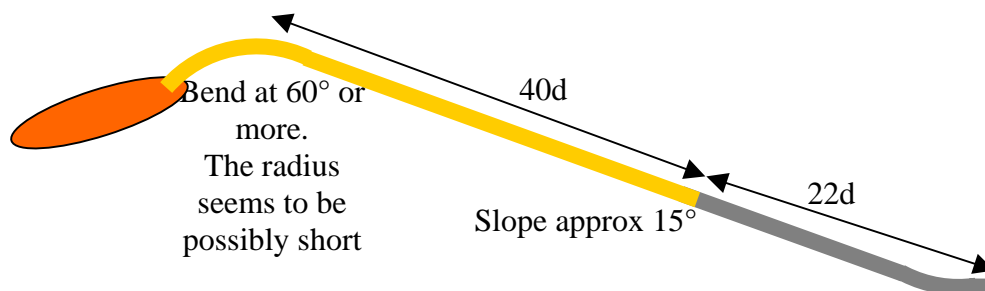
**Criteria to be fulfilled if possible:** Some of these criteria could evolve with the knowledge of pop-pop engines.

- (1) Evaporator able to store heat (constant power).
- (2) Evaporator able to restitute intermittently (almost instantaneously) much heat.
- (3) Nozzle (even if its diameter is the one of the pipe) horizontal in order to exert a horizontal thrust.
- (4) Long length of the pipe with slope down towards the nozzle to store the « water snake » and to limit the gas vents.
- (5) As few accidents as possible on the part of the pipe which contains liquid water to limit pressure losses.
- (6) Heat losses between hot source and cold one by conduction of the pipe to be limited.
- (7) Evaporator volume to be limited (because the thrust is inversely proportional).
- (8) Evaporator exit going up. In fact it is to ease the water drops climbing down towards the evaporator.
- (9) Length of the pipe from its upper point to the nozzle equal to approximately 62 times its diameter.
- (10) Distance between cold source and hot source to be approximately 40 times the diameter.

### Practical application:

- (1) (2) and (7) → Evaporator made of copper with large heated area and small volume.
- (5) → Long bending radius between nozzle and pipe.
- (6) → Upper part of the pipe to be thin and made of stainless steel, steel, possibly brass, but avoid aluminum and most of all copper.
- (10) → Lower part of the pipe made of copper or aluminum...or materials that are less heat conductor (for instance the one used in the upper part) if this lower part is immersed.

### Design:



The rest is to be decided by you as you feel it. Example (questionable):

